

High Pressure Reverse Osmosis shows promising perspectives for the Treatment of Electroplating Wastewater and Trivalent Chromium

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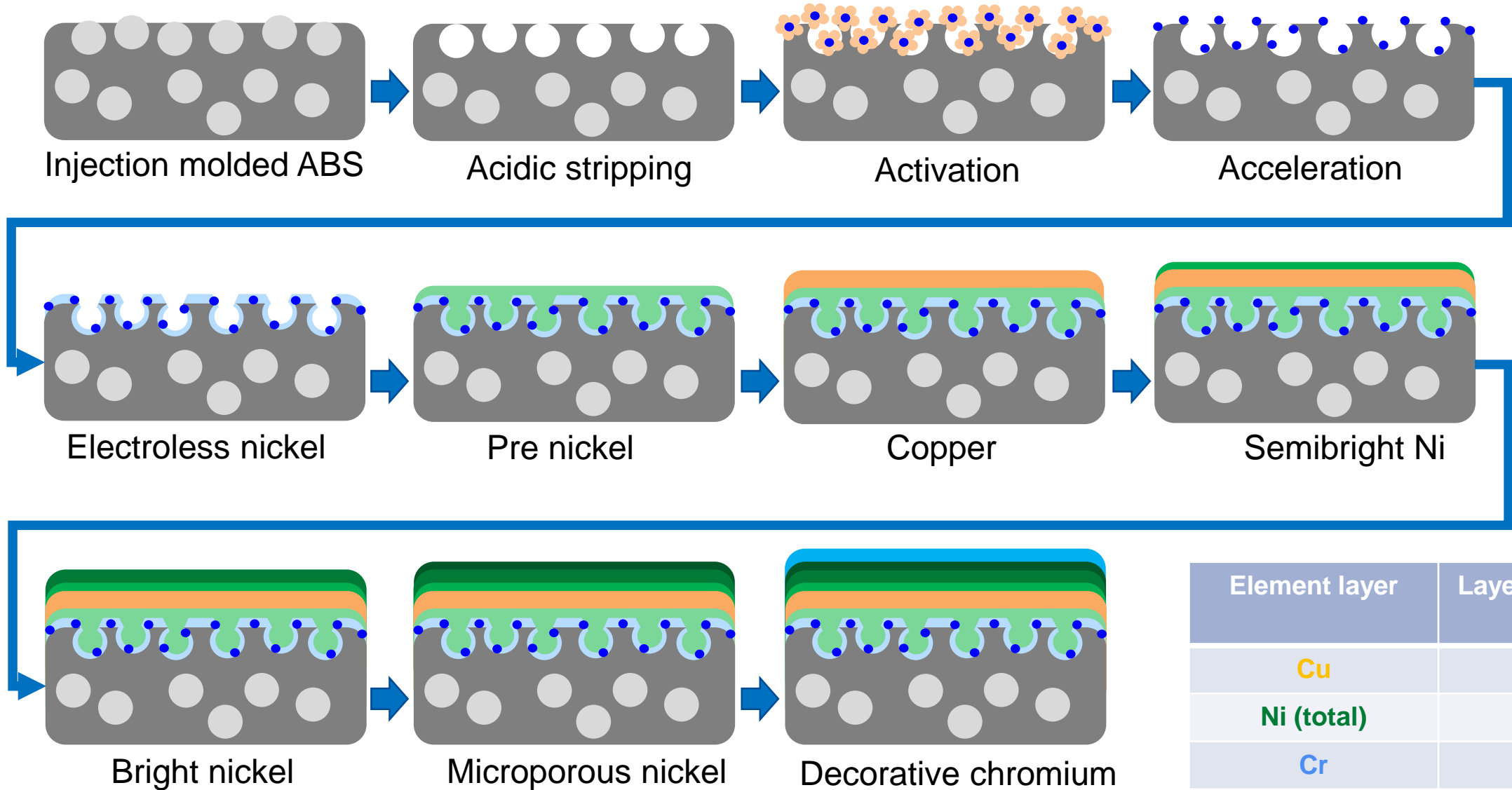
Outline

- **Electroplating plastics & the IntelWATT project**
- **Analysis of real Cr III) electroplating rinse waters**
- **Recovery of electrolyte: Reverse osmosis trials**
- **Concentrate Reuse: Electroplating tests via Hull cell tests**





The electroplating of ABS plastics



Element layer	Layer thickness / μm
Cu	25
Ni (total)	15
Cr	0.3-0.8



Electroplating line in Solingen, Germany



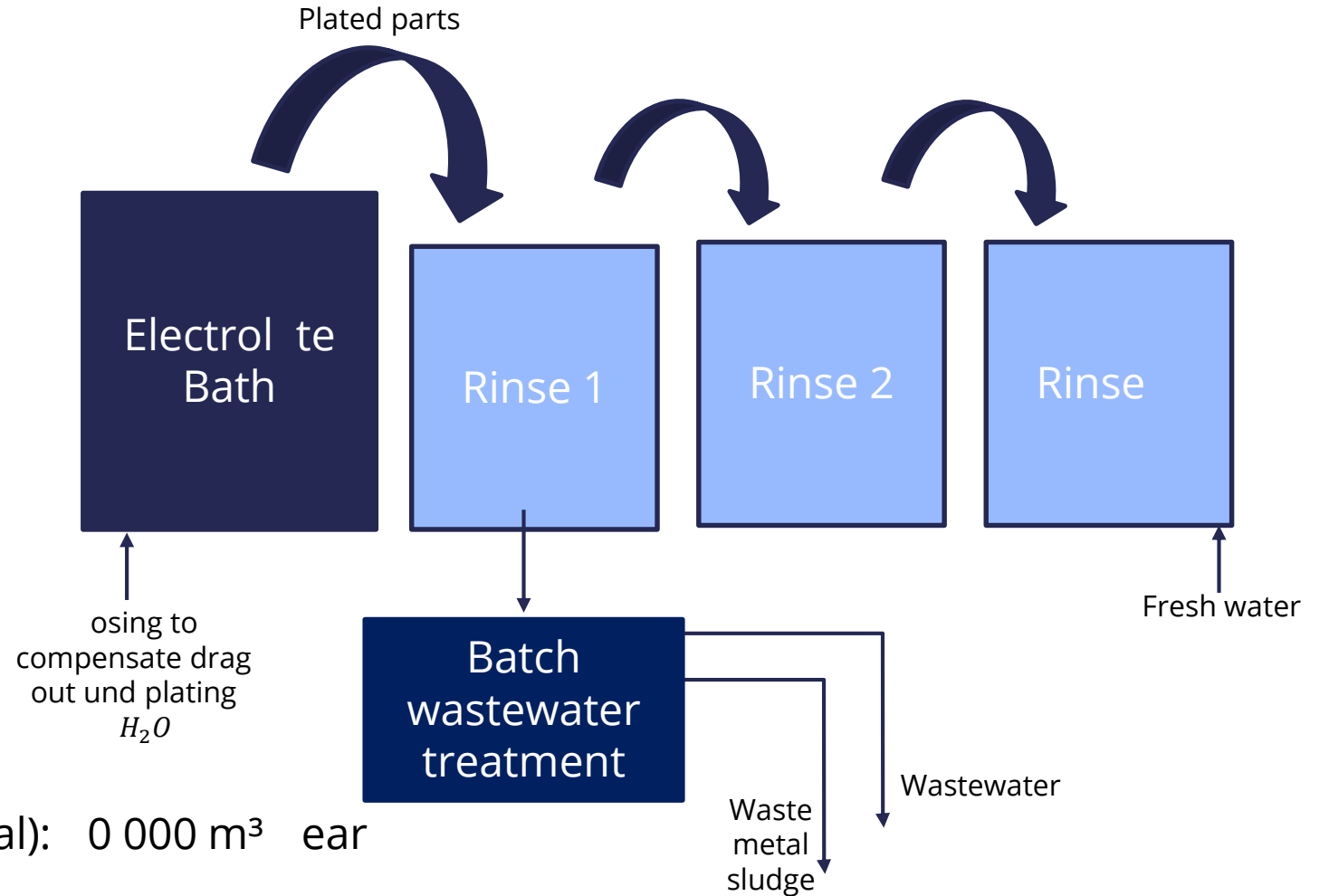
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intelWATT - Case Study 3

The waste water treatment to date



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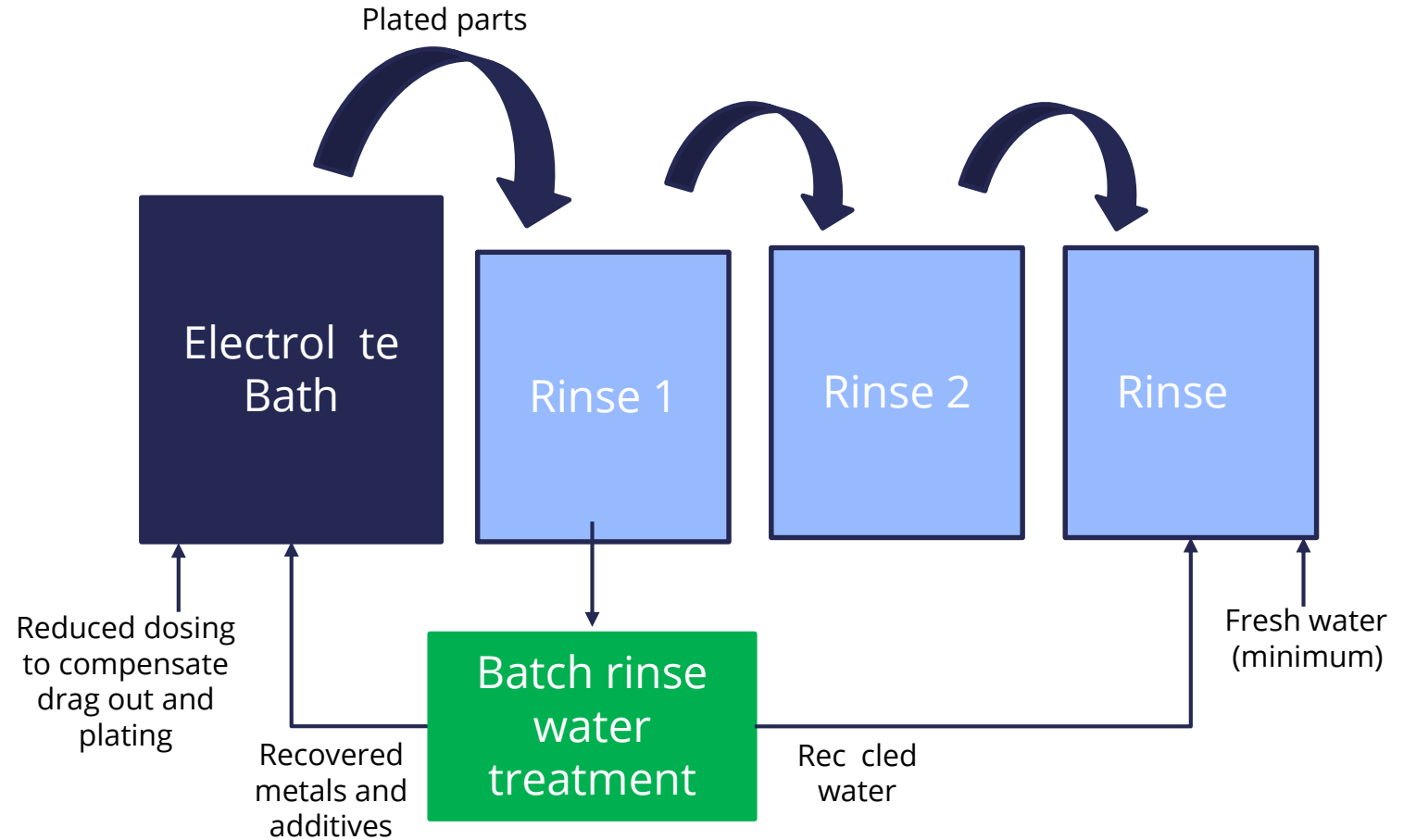
Needed rinse water b B GmbH (global): 0 000 m³ year

intelWATT - Case Study 3

The intelWATT approach



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Requirements

Quality parameters for RO permeate recycling in rinsing baths

Quality Parameter	Unit	Lower limit	Upper limit	Measurement Method
pH value		5	8	pH meter
Surface Tension	mN m	0	2	Tensiometer
Chromium ()	mg L	0	10	CP OES
Nickel	mg L	0		CP OES
Copper	mg L	0		CP OES
Boric cid	mg L	0	100	CP OES
Sulfate	mg L	0	150	CP OES Titration
Malic cid	mg L	0		HPLC
Chloride	mg L	0	50	Titration
Total Organic Carbon	mg L	0	15	ifference method

Quality parameters for RO concentrate* re-use in electroplating baths

Quality Parameter	Unit	Lower limit	Upper limit	Measurement Method
pH value		.5	.9	pH meter
Surface Tension	mN m	0	50	Tensiometer
Chromium ()	g L	8	12	CP OES
Nickel	mg L	0	15	CP OES
Copper	mg L	0		CP OES
Boric cid	g L	80	110	CP OES
Sulfate	g L	80	150	CP OES Titration
Malic cid	g L	0.	2.5	HPLC

equal to electroplating parameters

Cr(III) electrolyte recovery by RO: Predicted challenges and issues to overcome

- Unknown components and concentrations in real electroplating rinse water
- Surfactants blocking the membrane
- High TOC content: Fouling
- Cr stallization of boric acid on the membrane (solubilit limit 55 g L 25°C)
- Feed pH ≤ 5 : Low membrane rejection of protonated (neutral) boric acid



Quantification of main inorganic components in real electroplating rinse waters

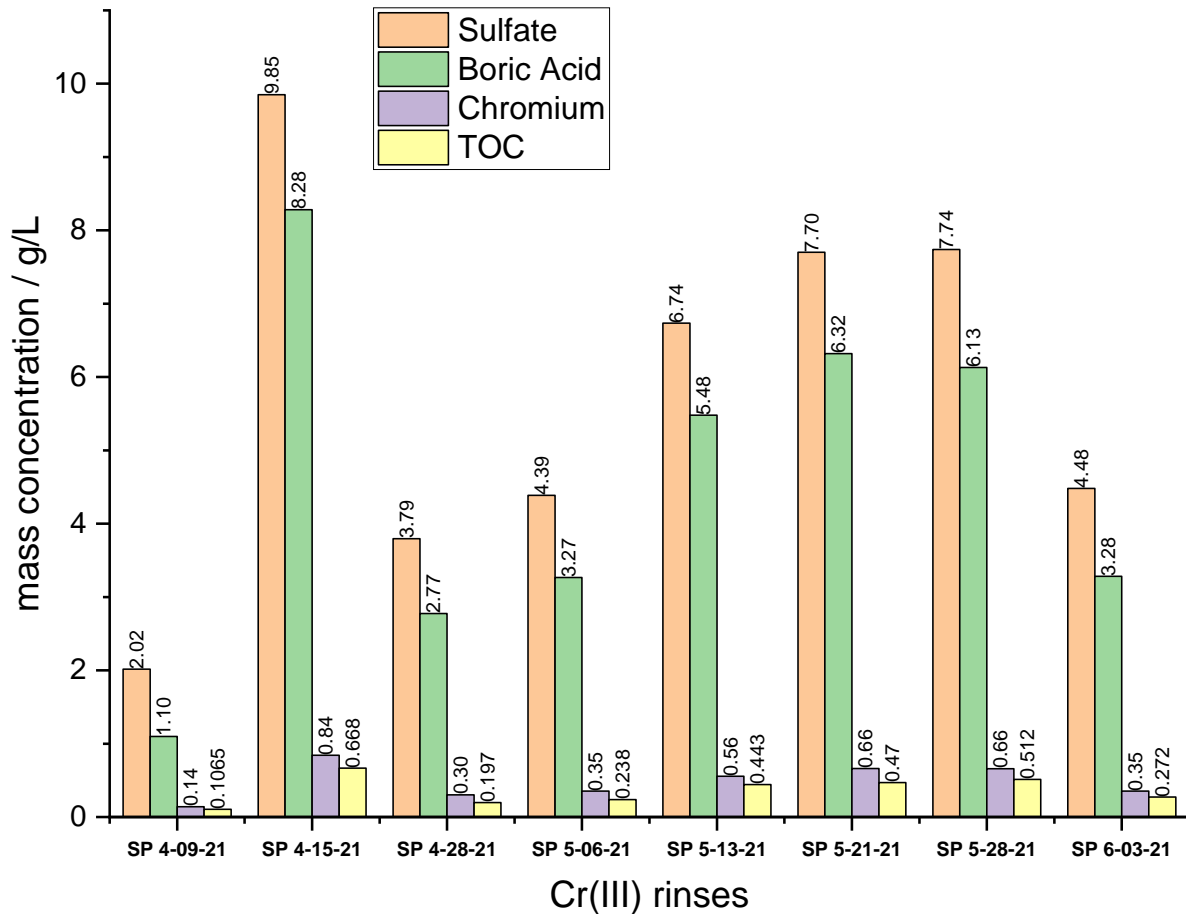
Via ICP-OES and TOC difference method

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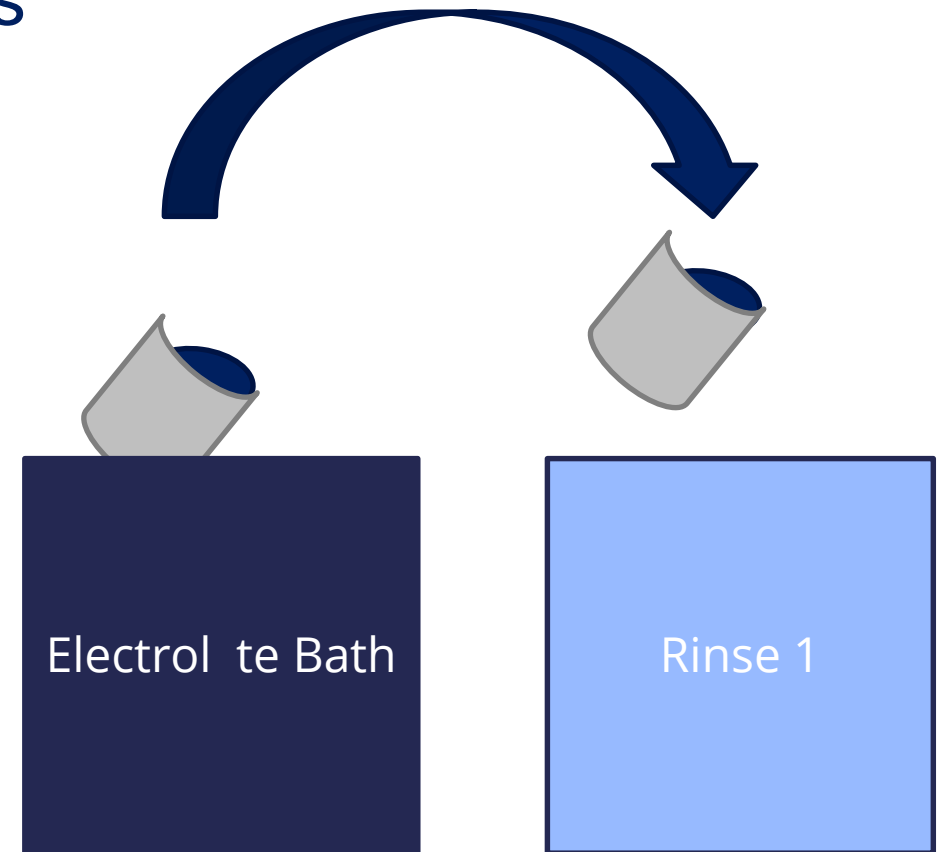
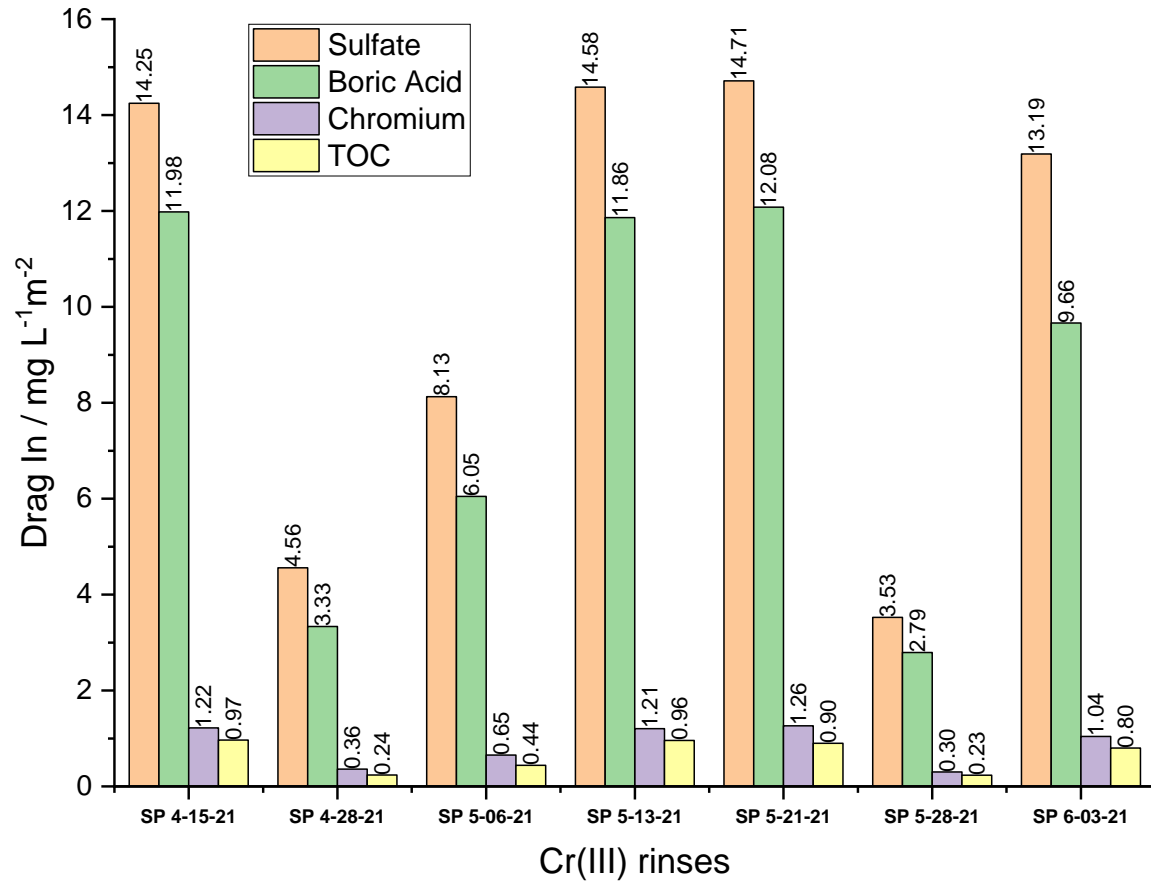


ICP-OES of real Cr(III) bath rinses + TOC



Sample	β_{Cr} / g/L	$\beta_{SO_4^{2-}}$ / g/L	$\beta_{B(OH)_3}$ / g/L	β_{Ni} / mg/L	TOC / mg/L
SP 4-09-2021	0.14	2.02	1.10	2.58	106.5
SP 4-15-2021	0.84	9.85	8.28	8.84	668
SP 4-28-2021	0.0	.9	2.	2.5	197
SP 5-06-2021	0.5	4.9	.2	.21	238
SP 5-13-2021	0.5	.4	5.48	4.2	443
SP 5-21-2021	0.	.0	.2	5.45	470
SP 5-28-2021	0.	.4	.1	5.48	512
SP 6-03-2021	0.5	4.48	.28	.9	272
$\bar{x} \pm \Delta x$	0.48 ± 0.23	5.83 ± 2.58	4.58 ± 2.35	4.60 ± 1.94	363.3

Relative drag-in of inorganic components





Reverse osmosis for the recovery of electrolyte from rinse water

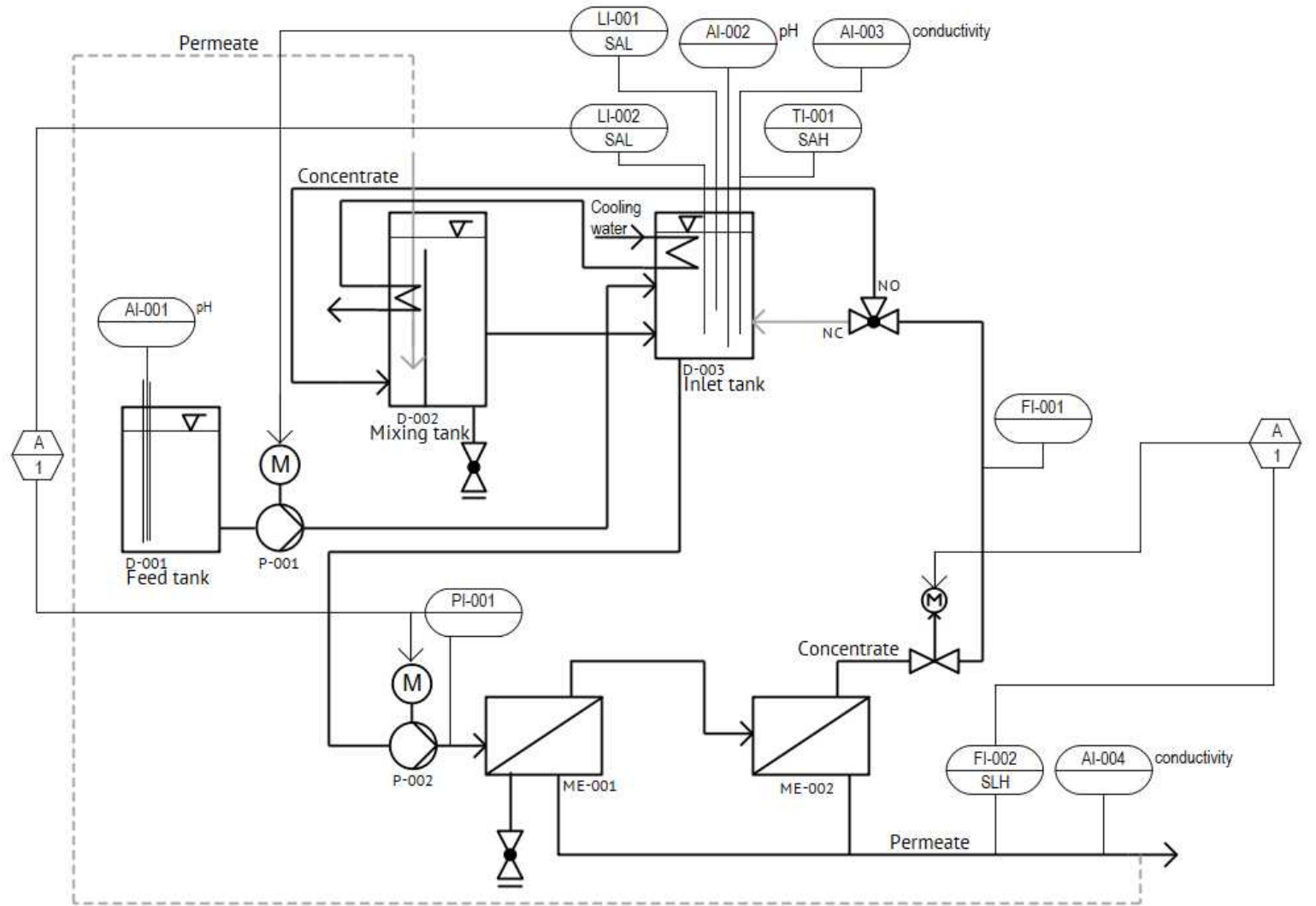
Characterization of the process

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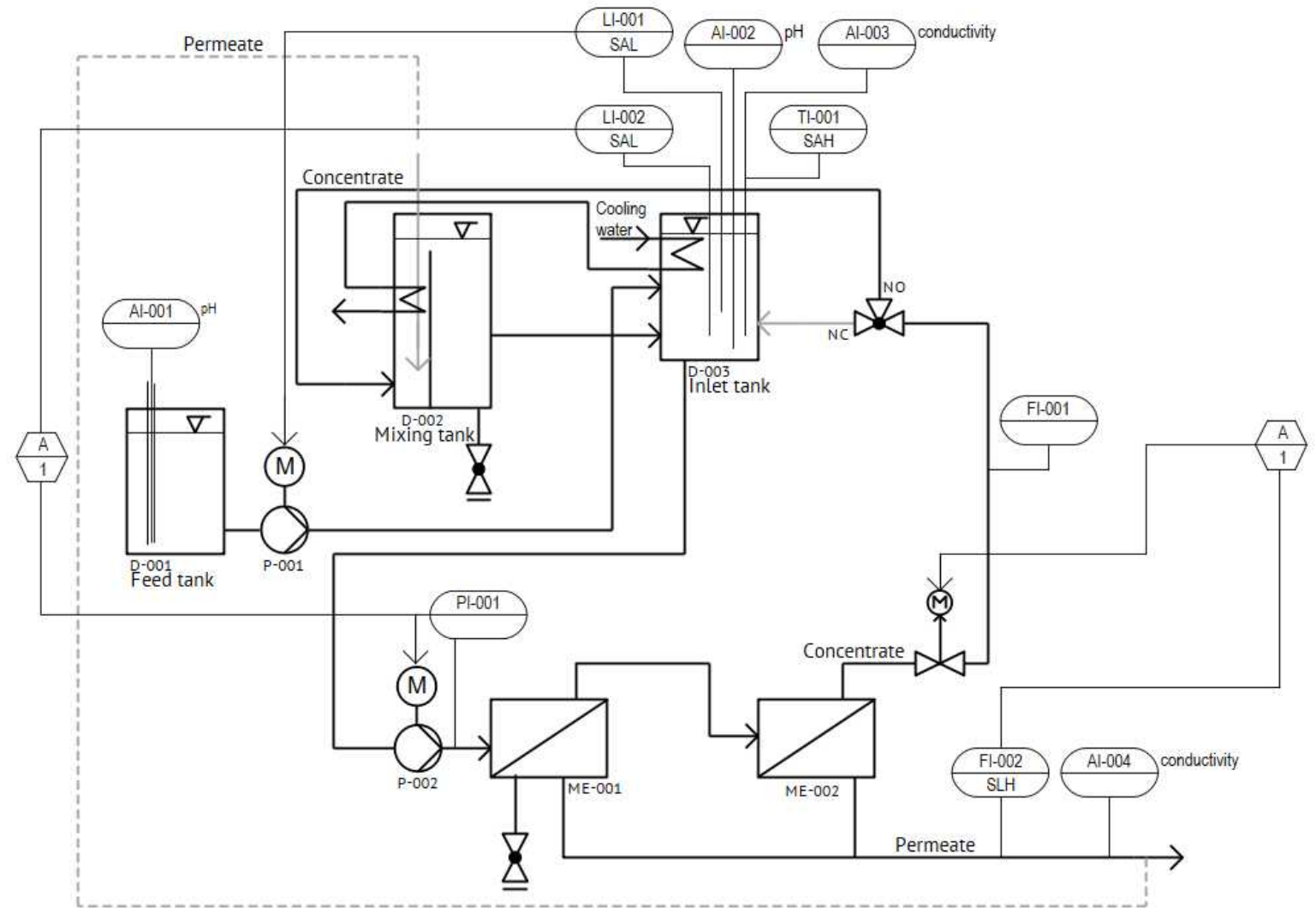
RO lab plant



RO trials

Parameter	Value
T °C	25
p_{max} bar	80
$pH_{initial}$	4.
J_{max} L m ² ·h	0
$v_{crossflow}$ m s	0.25
$A_{M;total}$ cm ²	1 0
$A_{plant;inner}$ cm ²	≈ 4251

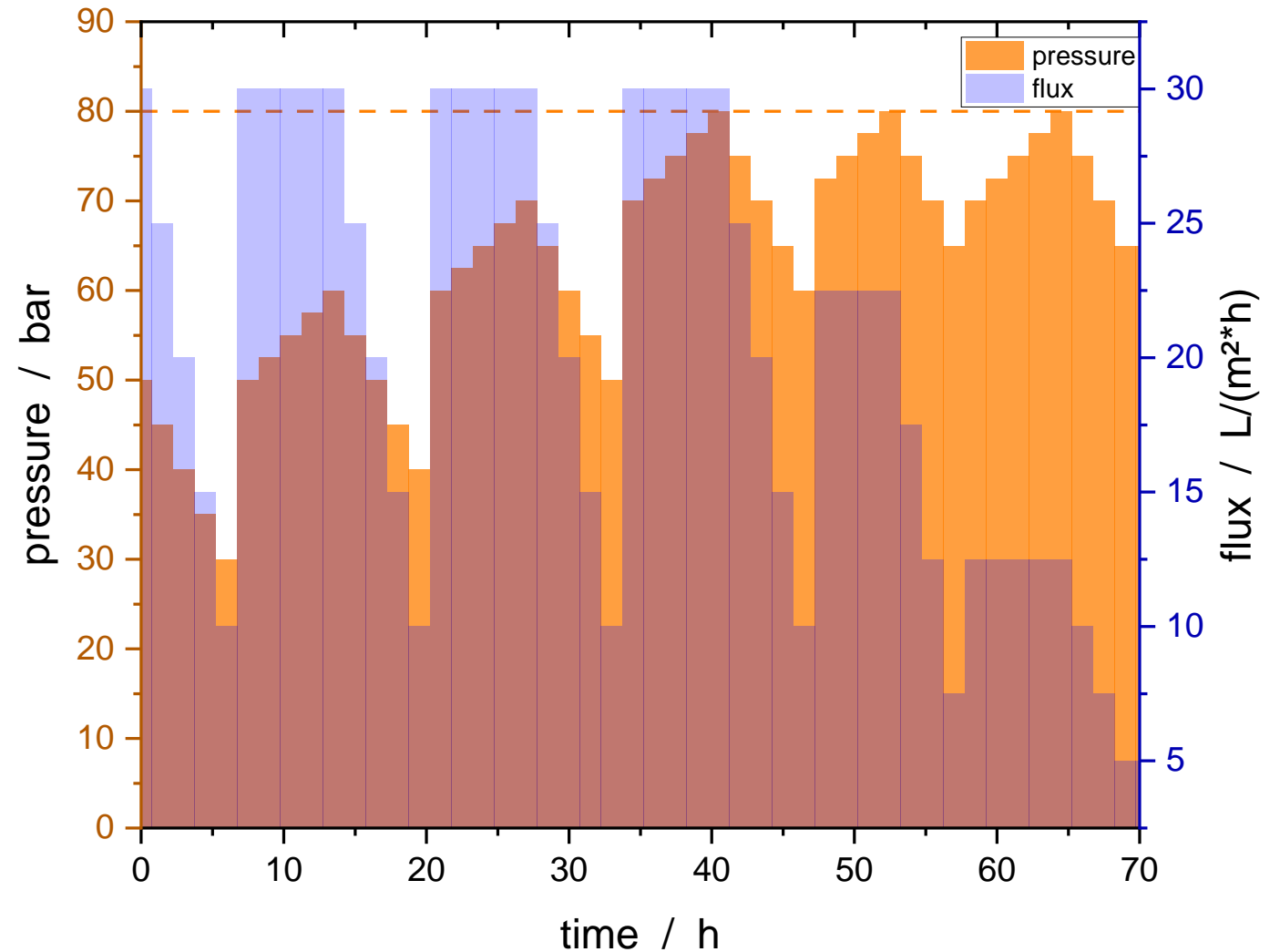
Feed: diluted Cr() Electrolyte
 (8 of initial concentration 0.5 g L Cr)
 Membrane: **SW30 DuPont-Filmtec**



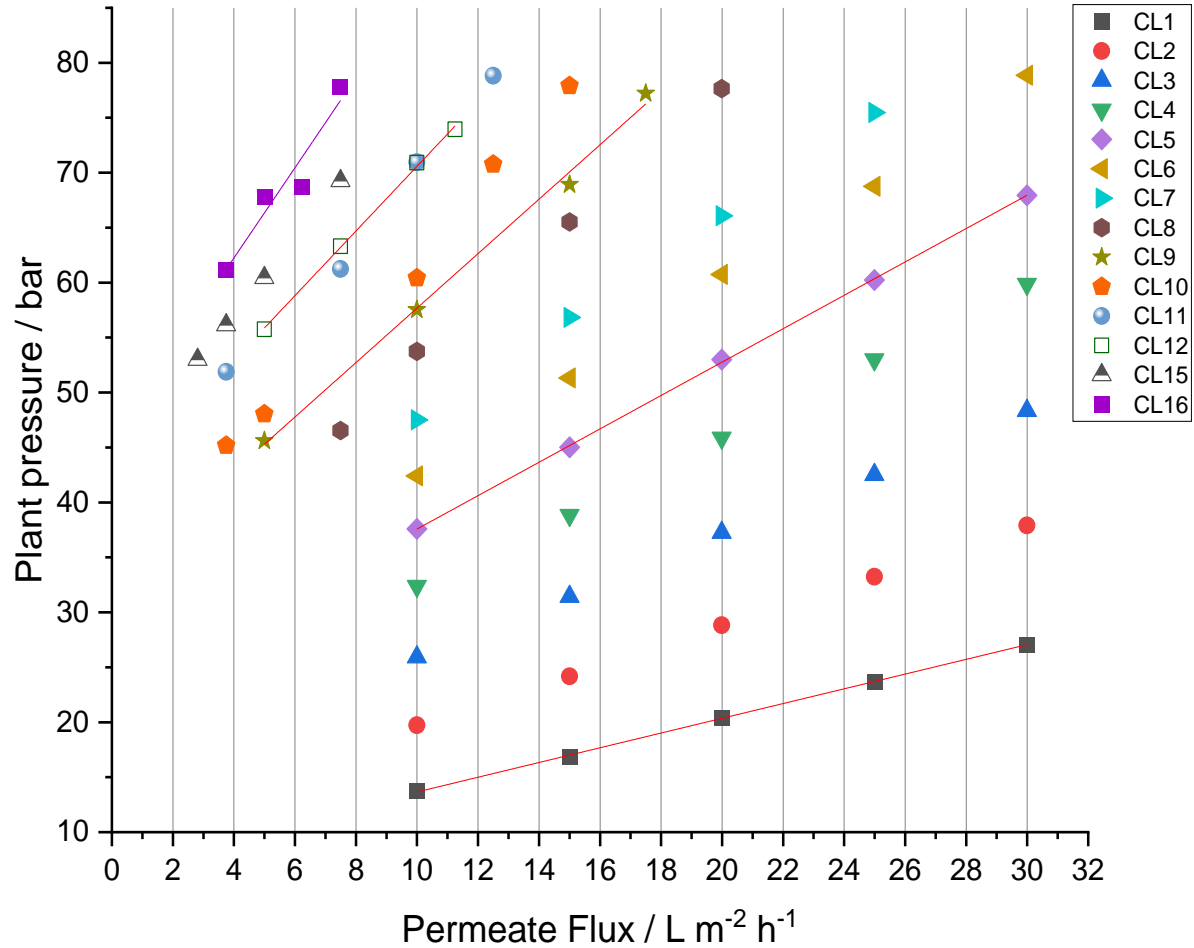
DOE: Increasing the concentration of artificial Cr(III) rinse water

Parameter	Value
T °C	25
p_{max} bar	80
$pH_{initial}$	4.
J_{max} L m ² ·h	0
$v_{crossflow}$ m s	0.25
$A_{M;total}$ cm ²	1 0
$A_{plant;inner}$ cm ²	≈ 4251

Feed: diluted Cr(III) Electrolyte
 (8% of initial concentration 0.5 g/L Cr)
 Membrane: **SW30 DuPont-Filmtec**

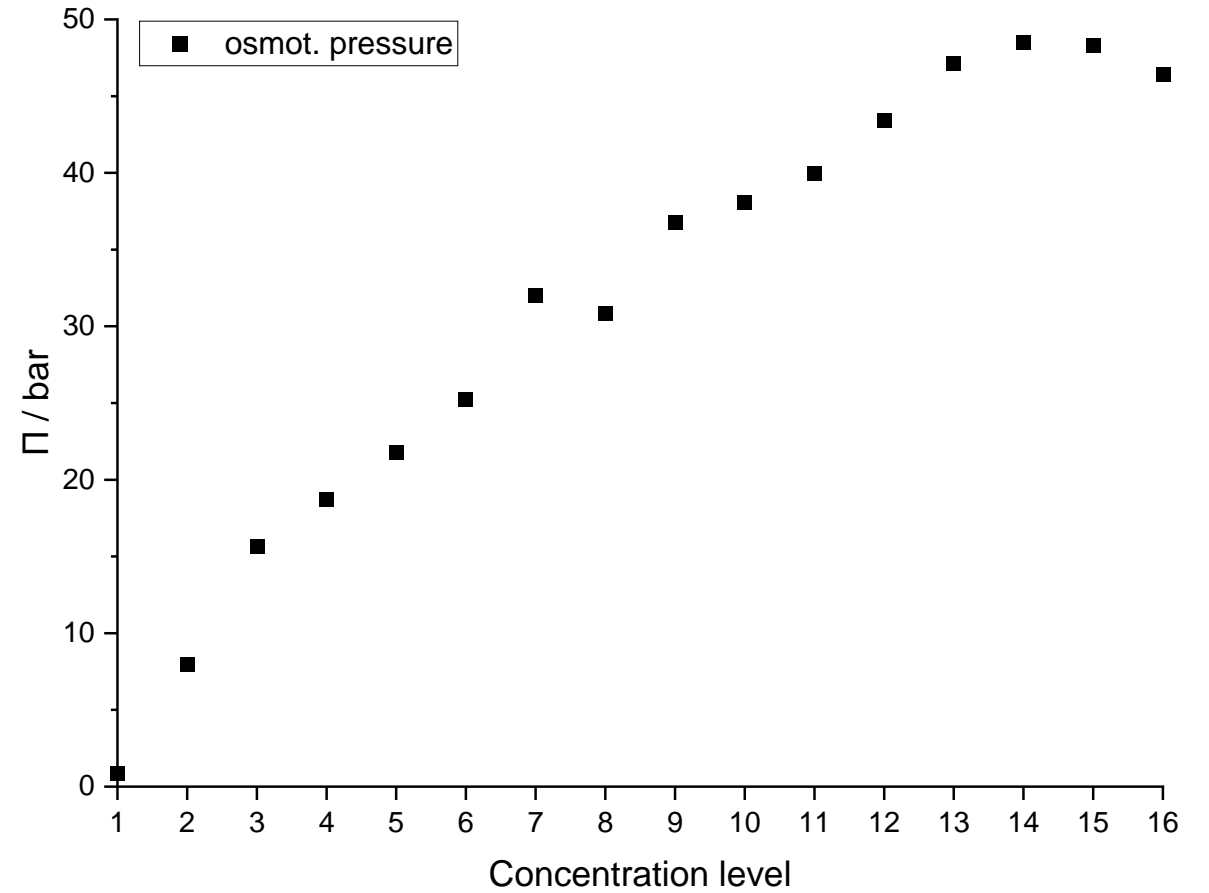


Plant Pressure-Flux diagram



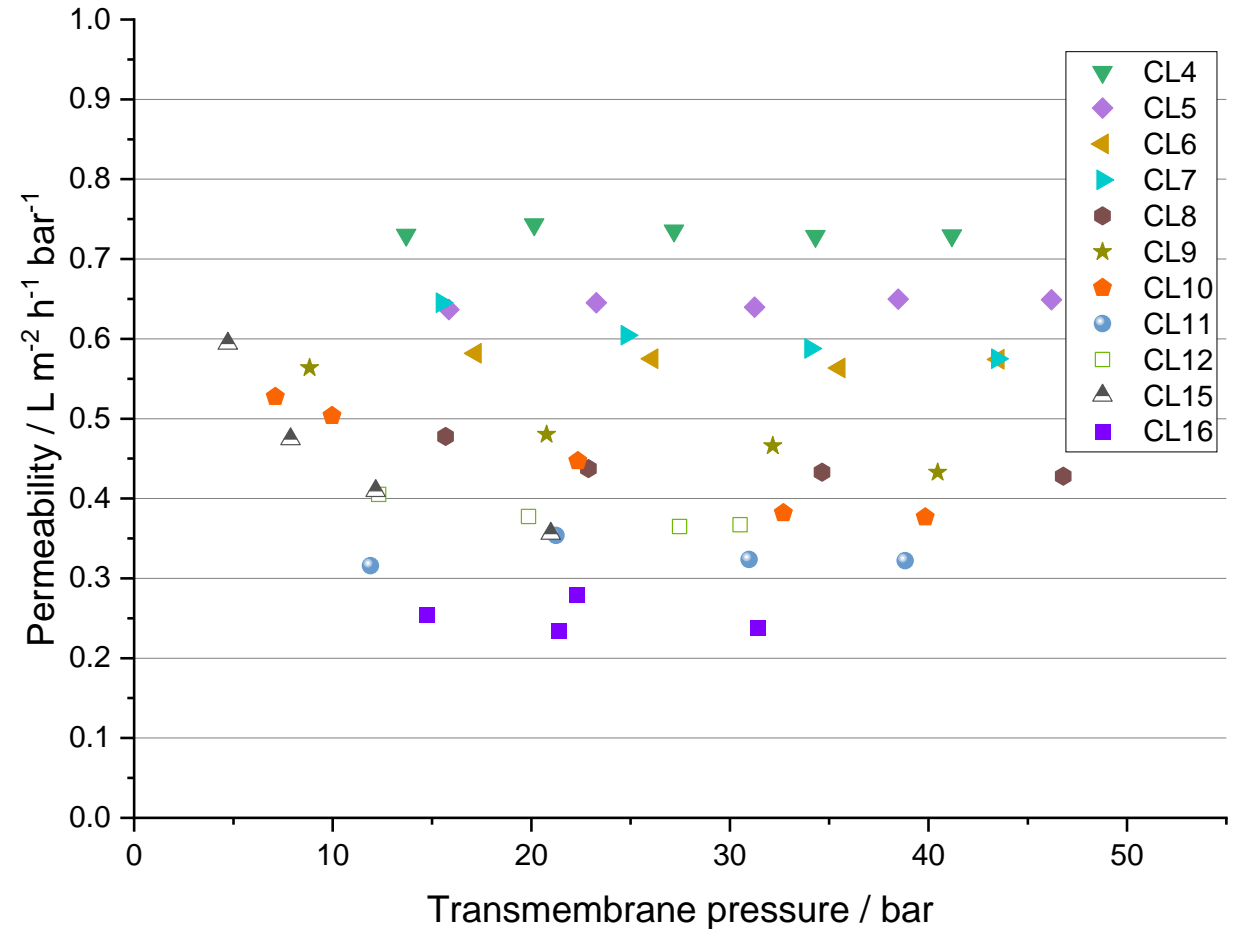
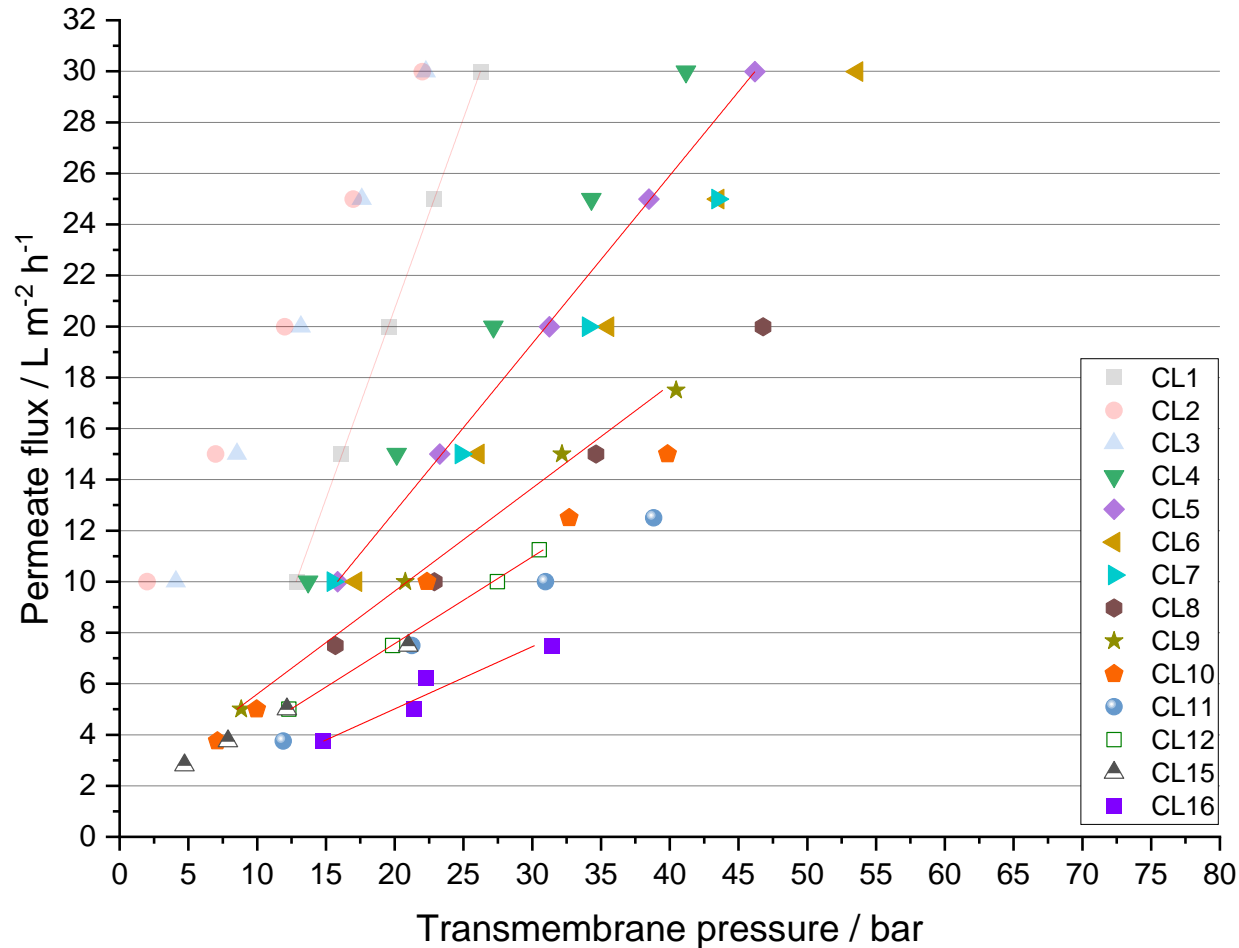
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Osmotic pressure of RO concentrates

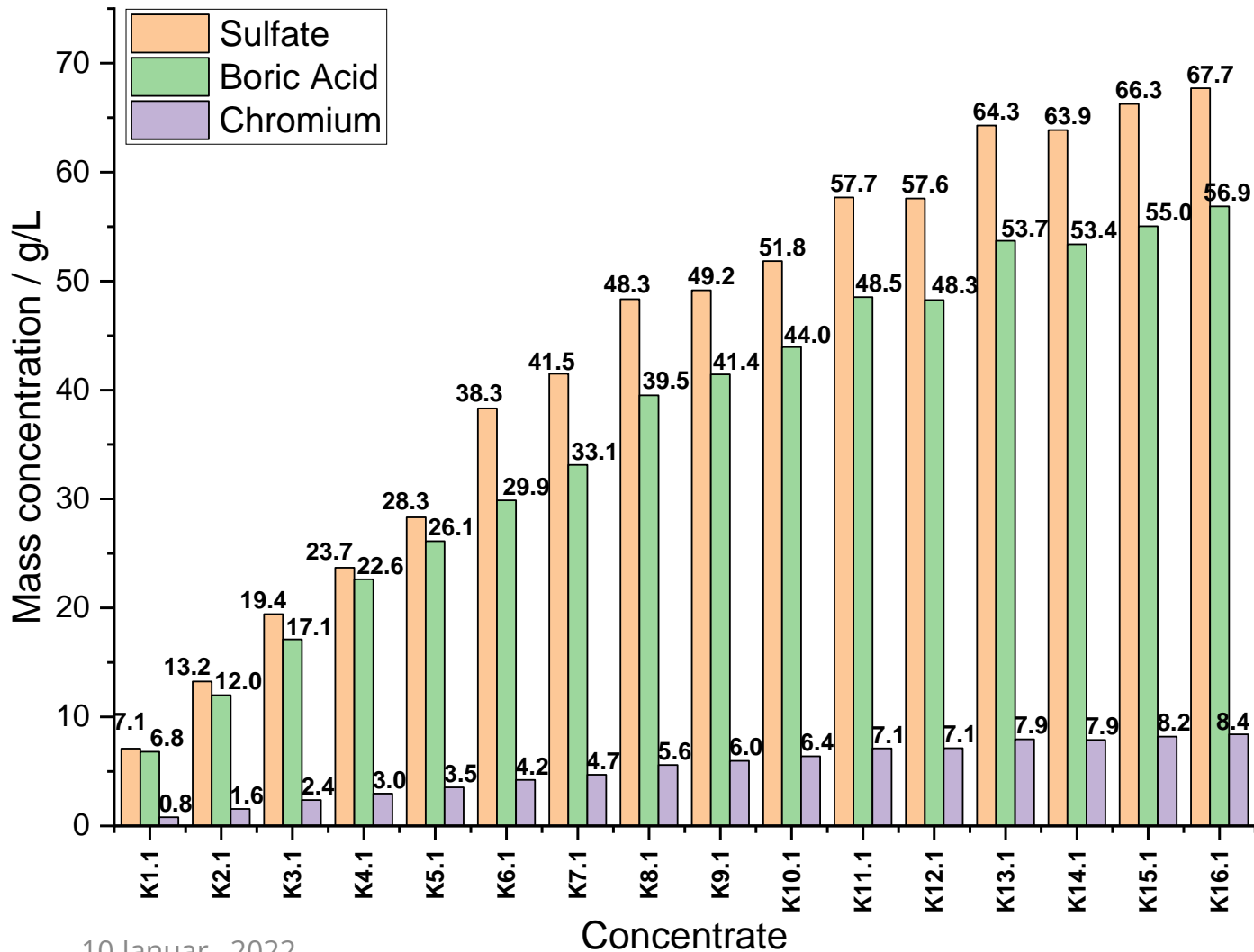


Measured with vapor pressure osmometer

Permeate flux and Permeability in dep. of the Transmembrane pressure



ICP-OES analysis of RO concentrates

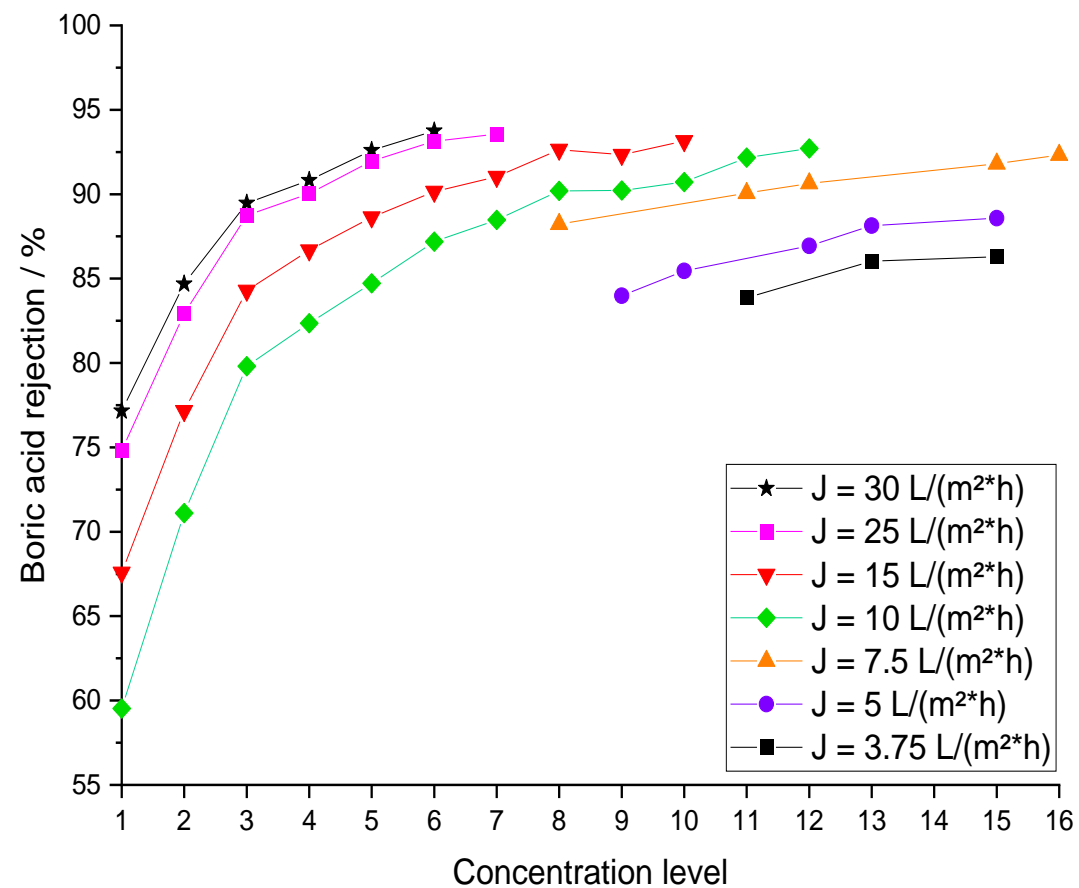
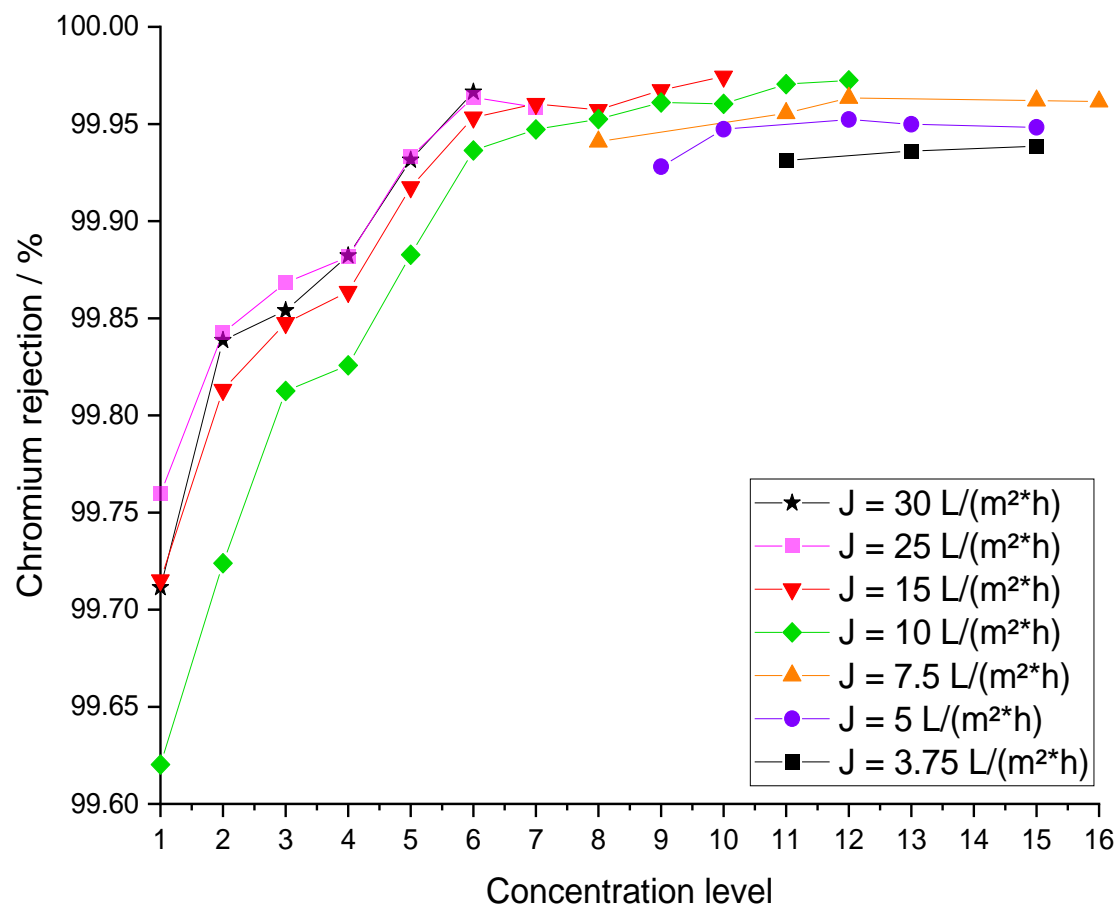


	β_{Cr} / g/L	$\beta_{B(OH)_3}$ / g/L	$\beta_{SO_4^{2-}}$ / g/L	γ / mN/m	pH
Cr III) Electrolyte	8-12	80-110	80-150	30-50	3.5-3.9
HPRO feed	0.75	3.55	7.12	72.0	4.7
Concentrate K16.1	8.39	56.89	67.72	63.7	3.85



Concentrate Permeate

Rejection of chromium and boric acid



RO membrane after use – fouling!



But: Pilot plant will run in batch: Cleaning is taken into account

	NaCl rejection / %	Permeate flux / $L m^{-2} h^{-1}$	Plant pressure / bar	Permeability / $L m^{-2} h^{-1} bar^{-1}$
Pre RO experiment	93.0	30.0	34.2	1.987
Post RO Experiment J(pre)=J(post)	98.3	30.0	55.4	0.826
Post RO Experiment p(pre)=p(post)	97.8	15.0	35.0	0.943

Tested with 2 NaCl solution $\Pi = 19.1 \text{ bar}$

Permeability calculated with transmembrane pressure ($= \Delta p - \Delta \Pi$)



Use of RO concentrate as recovered electrolyte in electroplating

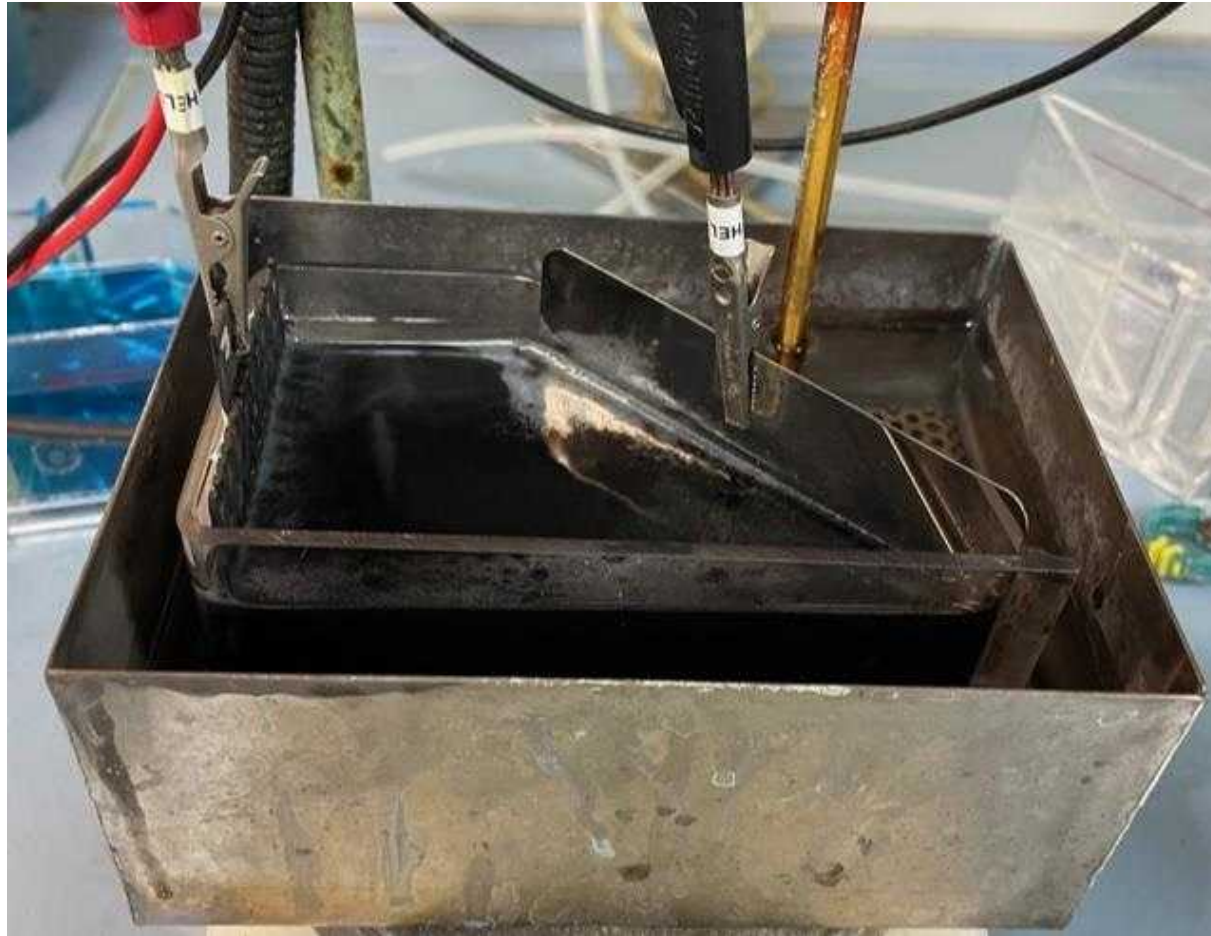
Hull cell tests

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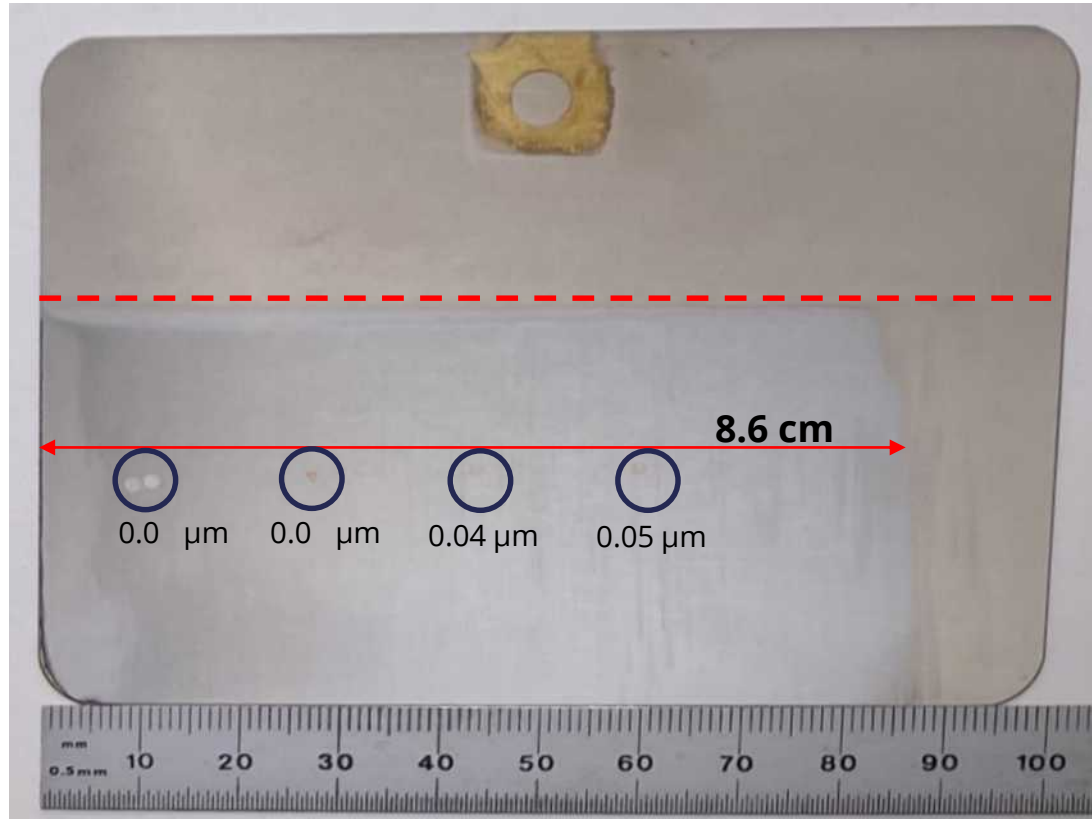
Hull Cell testing – Plating with RO concentrate



Parameter	
Current	5
Plating time	min
Temperature	55 °C
node	r Ta o ide coated titanium
Substrate	Plated on nickel coated brass panel (.5 cm 10 cm)
Volume	250 mL RO concentrate as electrolyte

Hull cell test plate analysis

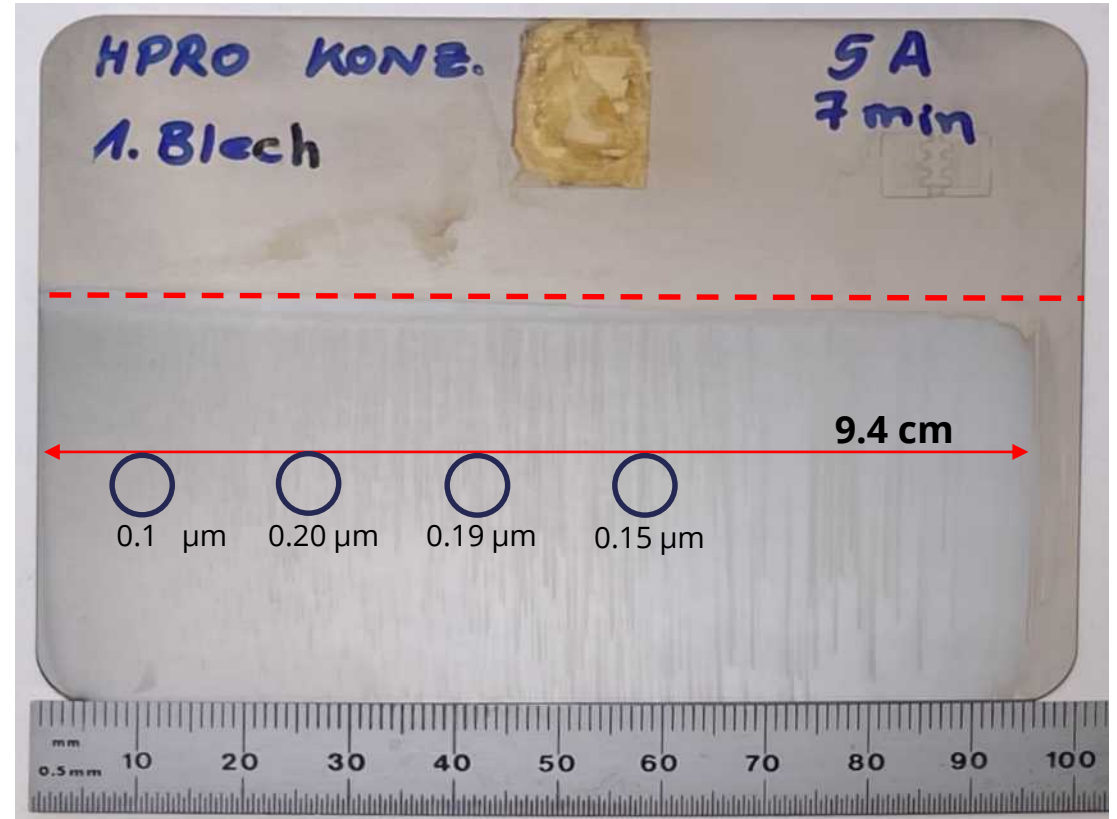
Concentrate initial



High current densit

Low current densit

Concentrate increased conc.



High current densit

Low current densit

Take home message

- Feasibility of RO treatment for Cr() rinse waters
 - Sufficient membrane rejection of Cr(): 99.95
 - RO 80 bars: sufficient concentrations for concentrate re use achieved
 - Boric acid conc. reached solubility limit without blocking the membrane

Outlook

- Need for treatment: Permeability of membrane decreases significantly
 - Cleaning step (backwashing)

Thanks to



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Thank you for your kind attention!

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